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Analysis of Multilayer Stacked Microstrip Patch Antenna for Bandwidth Enhancement

Nagendra Pachauri, Aparna Gupta and Soni Changlani

Dept. of Electronics and Communication Engineering, Laxmi Narayan College of Technology & Science Bhopal,

Madhya Pradesh, India

ABSTRACT: In this paper we design and simulate four types antenna with different dielectric material and compared result on the basis of variation of different dielectric coefficient and different layers and calculate some parameter of antenna for bandwidth analysis. We have enhance bandwidth of increasing layer that is 12.639%, 15.27%, 21.9% and 33.22% respectively up to forth layer.

KEYWORDS: Microstrip patch antenna; stacked Antenna, bandwidth.

I. INTRODUCTION

Microstrip antennas are in greater demands in wireless communication and space applications because of small size, low weight. The microstrip antennas possess the shortcomings such as narrow bandwidth, low gain and poor efficiency [1]. These shortcomings can be overcome by using multilayered rectangular microstrip antennas. This can be achieved by proper combination of the substrate and superstrate thickness over and under the patch. Multilayer Microstrip patch is also useful to provide protection to patch from heat, rain, physical damage, and naturally formed ice layers during flight [3]. There are many methods available in the literature to calculate the resonant frequency of multilayered rectangular patch based on numerical technique [2]. None of the efficient analytical model is available in literature related to multilayered structure to obtain the antenna dimension. There are mainly four techniques for enhancement of Bandwidth of given Microstrip Patch Antenna. Which are, multilayered configurations of Broadband Microstrip patch antenna, Stacked Multiresonator Microstrip patch antenna, Modified Shape Patch Broadband Microstrip patch antenna, Planar Multiresonator configuration of Broadband Microstrip patch antenna, in multilayered configuration patches are placed over different dielectric substrates and they are stacked on each other. Based on the coupling mechanism, these configurations are of two types electromagnetically-coupled or aperture-coupled. There are mainly two method of coupling to multilayered antenna, Electromagnetically-coupled Technique and Aperture-coupled Technique. In Stacked Multiresonator Microstrip patch antenna configuration multiresonator and stacked configurations are combined to provide broadband microstrip patch antenna. This antenna is applicable for wireless communication such as WLAN. A single line feed stacked microstrip antenna for 4G system is presented and performance of proposed antenna improvement of bandwidth 15% [4].

II. RELATED WORK

I. J. Bahl et. al [3] design of a microstrip antenna covered with a dielectric layer is presented. Due ton loading, the resonant frequency of the antenna changes. The absolute value of the change increases with the operating frequency, the relative permittivity (except plasma), and the thickness of the dielectric layer. This change may cause degradation in performance due to the inherent narrow bandwidth of microstrip antennas if the effect of loading is not considered in the design. The curves presented here may be used to design microstrip antennas that may be subjected to icing or a plasma environment or coated with protective layers. Numerical and experimental results for the fractional change in the resonant frequency are round to be in good agreement.



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[4] A single line feed stacked microstrip antenna for 4G system is presented by Awadhesh K. G. Kandu and D.C. Dhubkarya. The proposed antenna with two properly square patches are stacked. The top patch can perform as a driven element is design on 2.44 GHz and lower patch is also design on 2.44 GHz. The performance of proposed antenna for 4G band frequency (2400-2500 MHz). Also gating the improvement of bandwidth (15%) is very high compared to conventional antenna.

R. Afzalzadeh and R. N. Karekar [5] design a dielectric protecting superstate with spacing on the order of one wavelength from the rectangular microstrip patch antenna and of thickness up to about half a wavelength shows very small variation in resonance frequency (fr) and reflection coefficient (Γ). Effects of the same on radiation pattern (RP) includes drastic changes in beamwidths. By use of the spaced superstate the patch can be protected without the need to redesign parameters like fr and Γ .© 1994 John Wiley & Sons, Inc.

Shavit, R [6] A theoretical model to analyze a covered rectangular antenna with an arbitrary dielectric constant superstrate is developed. The antenna is simulated by the radiation of two magnetic dipoles located at the radiating edges of the patch. The Green's function of an elementary magnetic dipole in a superstrate-substrate structure, utilizing spectral-domain analysis, is formulated, and the surface-wave and radiation field are computed. An improved transmission line model, which considers the stored energy near the radiating edges and the external mutual coupling, is used to compute the input impedances and radiation efficiency. Design considerations on the superstrate thickness and its dielectric constant are discussed. Experimental data for a single element and a 4×4 microstrip array is presented to validate the theory.

N. Aouabdia et. al[7]worked on consists in characterizing a rectangular microstrip antenna while emphasizing the possibilities of various types of current expansion functions. A detailed calculation of the spectral Green's dyad, and conduction current calculated by the integral equation method via the moment's method was treated. The numerical method consists in simulating the various types of basic functions by testing convergence and by considering the effect of the parameters of the dielectric substrate such as thickness and permittivity on resonance frequency. An application of the air gap structure was also taken into account.

Ansari, J. A., Singh, P., & Yadav, N. P [8] analyses of stacked patch antenna with two parasitic elements is presented. The antenna shows improved radiation and directivity by 6.57 dB when compared with single layer patch antenna. The bandwidth of the antenna is found to be dependent on various parameters such as h_1 , h_2 , and s. The proposed results are compared with the IE3D simulation and reported experimental results.

Sharma, A., & Singh, G. [9] they are simulated a single-pin-shorted microstrip line fed three-dielectric-layer (with different permittivity and thickness) rectangular patch microstrip antenna for all those communication systems whose limited antenna size is premium. Low permittivity hard foam has been used as one substrate to achieve wide bandwidth. The simulation of this proposed antenna has been performed by using CST Microwave Studio, which is a commercially available electromagnetic simulator based on the finite difference time domain technique.

Liu, Z. F., et al [10] explained narrow bandwidth of a microstrip antenna is one of the important features that restrict its wide usage. A simple and practical method for the design of broad-band microstrip antennas is presented in this paper. Utilizing this design technique, several two-layer microstrip antennas have been proposed. To confirm the applicability of the method for the designs of antennas at L-band, experiments have been carried out. The measured results show that the proposed antennas have a bandwidth of up to 25.7%. Also, the method proposed in this paper is applicable to the design of other types of multilayered planar antennas.

J. A. Ansari et. al [11] analyzed of multilayer patch antenna has been carriedout. The antenna shows the broad bandwidth when a patch is stacked over fed patch in gap coupled structure. Typically a 42.65% bandwidth is achieved in three layer antenna. Further the bandwidth of the antenna depends inversely on the gap(s). The gain of the antenna is found to be 6.08 dB with 3 dB beam width of 92°. The theoretical results are compared with IE3D simulation and reported experimental data.



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Oluyemi P. [12] a novel design of a stacked-patch triple-band antenna in both circular and linear polarizations that can be used on a handheld terminal for surveying and geo-informatics applications is presented. The inculcation of corner truncation and I-slot in both the lower and middle patches has achieved better impedance bandwidth and axial ratio at GPS L1, L2, and GSM 1800 resonant frequency bands. A prototype of the proposed design is fabricated, and its performance is verified in measurement.

Samir Dev Gupta, M. C. Srivastava [13] described impedance bandwidth, one of the important characteristics of microstrip patch antennas, can be significantly improved by using a multilayer dielectric configuration. In this paper the focus is on bandwidth enhancement technique of a multilayer patch antenna for X-band applications. In order to enhance the bandwidth, antenna losses are contained by controlling those quality factors which can have a significant impact on the bandwidth for a given permittivity and thickness of the substrate. This has been achieved by conformal transformation of the multidielectric microstrip antenna. For the ease of analysis Wheelers transformation is used to map the complex permittivity of a multilayer substrate to a single layer. Method of Moments and Finite Difference Time Domain approaches are used for the computation of results.

III. ANALYSIS OF MULTILAYER MICROSTRIP PATCH ANTENNA

There are two way to calculate the value of effective dielectric for multilayers Microstrip antenna conformal mapping approach and transmission line approach but we used transmission line approach for analysis. The lowest-order mode, TM_{10} , resonates when the effective length across the patch is a half-wavelength. "Fig.1", demonstrates the patch fed below from a coaxial along the resonant length. Radiation occurs due to the fringing fields. These fields extend the effective open circuit (magnetic wall) beyond the edge. The resonance frequency f_{mn} depends on the patch size, cavity dimension, and the filling dielectric constant, as follows:

$$f_{mn} = \frac{k_{mn}c}{2\pi\sqrt{\varepsilon_r}} \tag{1}$$

Where m, n = 0, 1, 2... kmn = wave number at m, n mode, c is the velocity of light, \mathcal{E}_r is the dielectric constant of substrate, and

$$k_{mn} = \sqrt{\left(\frac{m\pi}{W}\right)^2 + \left(\frac{n\pi}{L}\right)^2}$$

(2)

For TM_{01} mode, the length of non-radiating microstrip patch's edge at a certain resonance frequency and dielectric constant according to equation (1) becomes

$$L = \frac{c}{2f_r \sqrt{\varepsilon_r}}$$
(3)
$$W = \frac{c}{f_r} \sqrt{\frac{2}{\varepsilon_r + 1}}$$
(4)

Where f_r = resonance frequency at which the rectangular microstrip antennas are to be designed. The radiating edge W, patch width, is usually chosen such that it lies within the range L<W>2L, for efficient radiation. The ratio W/L = 1.5 gives good performance according to the side lobe appearances. In practice the fringing effect causes the effective distance between the radiating edges of the patch to be slightly greater than L. By using above equation we can find the value of actual length of the patch as,



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Fig. 1 Multilayer Microstrip Antenna [13].

(5)

$$L = \frac{c}{2f_r \sqrt{\varepsilon_{eff}}} - 2\Delta l$$

Where ε_{eff} = effective dielectric constant and Δl = line extension which is given multilayered substrate material transmission line is shown in Figure 2.In this figure, a microstrip transmission line of length l, width w, and conductor thickness t is shown. However, each layer has different relative dielectric permittivity and substrate thickness as shown in the figure. In the case of multilayered substrate microstrip transmission line, the individual layer shave different relative dielectric permittivity, and overall relative dielectric permittivity of the substrate is presented by ε_{rc} and the value of ε_{rc} for a two-layered substrate material has been obtained in[14]. Similarly, the expression for the frequency dependent effective relative dielectric permittivity has been obtained in[15]. These two concepts are merged to obtain the mathematical expression for the frequency-dependent effective relative dielectric permittivity of the multilayered substrate material transmission line. The expression for the effective dielectric permittivity of the multilayered substrate material is expressed as using the following.





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(10)

$$d_{n} = \frac{K(k_{n})}{K'(k_{n})} - \frac{K(k_{n-1})}{K'(k_{n-1})} - \dots - \frac{K(k_{1})}{K'(k_{1})}$$

and in general

$$k_{n} = \frac{1}{\cosh\left(\frac{\pi w}{4(h_{n} + h_{n-1} + h_{n-2} + \dots + h_{1})}\right)}$$
 for n=1,2,3..... (11)

In the above equations, $h_n, h_{n-1}, \ldots h_1$ represents the individual substrate layer thickness starting from the top layer. Further, $\varepsilon_n, \varepsilon_{n-1}, \ldots, \varepsilon_1$ are the complex relative dielectric permittivity of the respective substrate layer. Where

$$\frac{K(k_n)}{K'(k_n)} = \frac{1}{\pi} \ln \left(2 \frac{1 + \sqrt{k_n}}{1 - \sqrt{k_n}} \right)$$
for $0.7 \le k_n \le 1$ (12)
With the help of Eq.(6) (12) the frequency independent relative dielectric

With the help of Eqs.(6)–(12), the frequency-independent relative dielectric permittivity of the multilayer substrate material(ε_{rc}) is obtained. Once this parameter is obtained, the next goal is to find the frequency-dependent behavior. The frequency-dependent behavior of a single-layered substrate material micro- strip transmission line is obtained with the help of the mathematical expression discussed in detail in [17, 18]. However, in the present case, as the multilayered Substrate relative dielectric permittivity has been reduced to ε_{rc} , it can be treated as the relative dielectric permittivity of a single substrate layer of thickness

 $h = h_n + h_{n-1} + \dots + h_1$ and is obtained with the following formulas

$$\varepsilon_{e}(f) = \varepsilon_{rc} - \frac{\varepsilon_{rc} - \varepsilon_{e}(0)}{1 + \left(\frac{f}{f_{a}}\right)^{m}}$$
(13)

$$f_a = \frac{J_b}{0.75 + (0.75 - 0.332 \varepsilon_{rc}^{-1.73})w/h}$$
(14)

$$f_b = \frac{47.746}{h\sqrt{\varepsilon_{rc} - \varepsilon_e(0)}} \tan^{-1} \varepsilon_{rc} \sqrt{\frac{\varepsilon_e(0) - 1}{\varepsilon_{rc} - \varepsilon_e(0)}}$$
(15)

$$m = m_0 m_c \tag{16}$$

$$m_0 = 1 + \frac{1}{1 + \sqrt{\frac{w}{h}}} + 0.32 \left(1 + \sqrt{w/h}\right)^{-3}$$
(17)

$$m_{c} = \begin{cases} 1 + \frac{1.4}{1 + w/h} \left(0.15 - 0.235e^{-0.45f/f_{a}} \right) & for \quad w/h \le 0.7 \\ 1 & for \quad w/h > 0.7 \end{cases}$$
(18)

$$\varepsilon_{e}(0) = \frac{\varepsilon_{rc} + 1}{2} + \frac{\varepsilon_{rc} - 1}{2} \left(1 + \frac{12h}{w} \right)^{-1/2} + F(\varepsilon_{rc}, h) - 0.217(\varepsilon_{rc} - 1) \frac{t}{\sqrt{wh}}$$
(19)
$$F(\varepsilon_{rc}, h) = \begin{cases} 0.02(\varepsilon_{rc} - 1)(1 - w/h)^{2} \text{ for } w/h < 1 \\ 0 & \text{for } w/h \ge 1 \end{cases}$$
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In the above expressions, $h = h_3 + h_2 + h_1$, w, and t are the total substrate thickness, width of the transmission line, and the thickness of the conductor, respectively. In the analysis, the absolute value of d has been taken in to the consideration because for three or more substrate layers, the value of dn as shown in(19)may be negative. However, its value should remain positive to represent the distance between two parallel plates of the equivalent capacitance model of the substrate.

IV. DESIGN AND SIMULATION OF PROPOSED ANTENNA

The proposed antennas designed frequency of 2.44 GHz, taking four types of dielectric constant of the substrate, RT Duriod (ε_r) = 2.2, glass epoxy= 4.2, woven Teflon fiber glass = 2.55, Ceramic= 28.2. The height of dielectric substrate (h) = 1.588 mm, 1.6 mm, 1.6 mm, 4.75 mm respectively. We have design four different antenna with different dielectric constant and calculated effective dielectric then design different Microstrip antenna.

(a) Designing of Microstrip Antenna with First Layer

The basic design parameter as design frequency 2.44 GHz, thickness of the patch 1.6 mm and dielectric coefficient of substrate is 2.55. Putting these parameters in above and can be calculated effective dielectric with help of two approach but we put in transmission line approach and calculate length of the patch 29.8 mm and value of width 38.125 mm. The dimension of the feed line calculated directly from the line Gauge of Zeland software for matching 50 Ω , are 21 mm × 4.47 mm and bottom side of patch consider to $W_g = W+6h$ and $L_g = L+6h$. The design parameters of the patch are indicated in Table 1.

Parameters	Specification	Unit	
Patch width	W	38.125 mm	
Patch length	L	29.8 mm	
Feed line length	F	21 mm	
Strip width	Т	4.47 mm	
Ground Plane width	\mathbf{W}_{g}	70 mm	
Ground Plane length	Lg	60 mm	
Cut width	W _C	6 mm	
Cut depth	D _C	6.5 m	
		m	

Table 1: Design parameters of single layer microstrip antenna.

(b) Simulation of Antenna with First Layer by IE3D

Making use of the IE3D software directly and select the Mgrid file, After the selection of Mgrid file then open basic parameter box and select the grid size 0.025 mm, meshing frequency 5 GHz and cell per wavelength = 20, then feed the some parameter before simulation in this dialog box like as top of the surface taking 1.6 mm, dielectric constant taking 2.55, and loss tangent taking 0.025. After the feed above parameters draw the finite ground plane with dimension 60 x 70 mm. Now draw the rectangular shape of length 29.8 mm and width 38.125 mm. After draw the patch select the edge of the patch and cut width of cut is 6 mm and depth of cut is 6.5 mm, now draw a straight line with length of 21 mm and width 4.47 mm. After the completion of designing select feed point location and feed at 29.1 mm in \times direction and 0 mm in y direction.



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Fig. 3 Proposed antenna with first layer at 2.44 GHz.

Simulation start with meshing frequency 5 GHz and the range of simulation frequency 0 - 5 GHz with step size 0.01 select the scheme as classical and enable adaptive symmetric matrix solver, simulation engine set as IE3D Full-Wave EM Engine, enable current distribution and radiation pattern, then select ok. After simulation all data are save in software directory.

(c) Designing of Microstrip Antenna with Second Layer

The basic design parameter as design frequency 2.44 GHz, thickness of the patch 1.6 mm, and 1.6 mm with dielectric coefficients of substrate are 2.55 and 4.2. Putting these parameter in transmission line approach and calculate length of the patch 29.6 mm and value of width 38.125 mm. The dimension of the feed line calculated directly from the line Gauge of Zeland software for matching 50 Ω , are 21 mm × 4.47 mm and bottom side of patch consider to W_g = W+6h and L_g = L+6h. The design parameters of the patch are indicated in Table 2.

Parameters	Specifications	Unit	
Upper patch width	W	38.125 mm	
Upper patch length	L	29.6 mm	
Feed line length	F	21 mm	
Strip width	Т	4.47 mm	
Ground plane length	L_{g}	60 mm	
Ground plane width	W _g	70 mm	
Cut width	Ŵc	6 mm	
Cut depth	D _C	6.5 mm	

Table 2: Design parameters of second layer antenna at 2.44 GHz.

(d) Simulation of antenna with second layer by IE3D

Making use of the IE3D software directly and select the Mgrid file, After the selection of Mgrid file then open basic parameter box and select the grid size 0.025 mm, meshing frequency 5 GHz and cell per wavelength = 20, then feed the some parameter before simulation in this dialog box like as top of the surface taking 1.588 mm, dielectric constant taking 2.55, and loss tangent taking 0.025, Again taking dielectric constant for second layer 4.2 and loss tangent 0.2. After the feed above parameters draw the finite ground plane with dimension 60 x 70 mm. After the feed above parameters draw the rectangular shape of length 29.6 mm and width 38.125 mm. After draw the patch select the edge of the patch and cut width of cut is 6 mm and depth of cut is 6.5 mm, now draw a straight line with length of 21 mm and width 4.47 mm. After the completion of designing select feed point location and feed at 29.1 mm in × direction and 0 mm in y direction.



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Fig. 4 Proposed antenna with second layer at 2.44 GHz.

Simulation start with meshing frequency 5 GHz and the range of simulation frequency 0 - 5 GHz with step size 0.01 select the scheme as classical and enable adaptive symmetric matrix solver, simulation engine set as IE3D Full-Wave EM Engine, enable current distribution and radiation pattern, then select ok. After simulation all data are save in software directory.

(e) Designing of Microstrip antenna with third layer

The basic design parameter as design frequency 2.44 GHz, thickness of the patch for first layer 1.6 mm, for second layer 1.6 mm and for third layer 4.75 mm and dielectric coefficient of substrate are 2.55, 4.2 and 28.2 respectively. Putting these parameters in above equation and calculate length of the patch 26.8 mm and value of width 38.125 mm. The dimension of the feed line calculated directly from the line Gauge of Zeland software for matching 50 Ω , are 21 mm × 4.47 mm and bottom side of patch consider to $W_g = W+6h$ and $L_g = L+6h$. The design parameters of the patch are indicated in Table 3.

Parameters	Specification	Unit	
Patch width	W	38.125 mm	
Patch length	L	26.8 mm	
Feed line length	F	21 mm	
Strip width	Т	4.47 mm	
Ground Plane width	\mathbf{W}_{g}	85.825 mm	
Ground Plane length	L_{g}	74.5 m	
		m	

Table 3: Design parameters third layer antenna at 2.44 GHz.

(f) Simulation of antenna with third layer by IE3D

Making use of the IE3D software directly and select the Mgrid file, After the selection of Mgrid file then open basic parameter box and select the grid size 0.025 mm, meshing frequency 5 GHz and cell per wavelength = 20, then feed the some parameter before simulation in this dialog box like as top of the surface taking 1.6 mm for first layer 1.6 mm for second layer and for third layer 4.75 mm with dielectric constant taking 2.55, 4.2 and 28.2 and loss tangent taking 0.025, 0.2 and 0.5 respectively. After the feed above parameters draw the rectangular shape of length 26.8 mm and width 38.125 mm. After draw the patch select the edge of the patch and cut width of cut is 6 mm and depth of cut is 6.5 mm, now draw a straight line with length of 21 mm and width 4.47 mm. After the completion of designing select feed point location and feed at 29.1 mm in × direction and 0 mm in y direction. On the bottom side of the lower patch design with 74.5 mm × 85.825 mm ground plane.



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Fig. 5 Proposed antenna with third layer at 2.44 GHz.

Simulation start with meshing frequency 5 GHz and the range of simulation frequency 0 - 5 GHz with step size 0.01 select the scheme as classical and enable adaptive symmetric matrix solver, simulation engine set as IE3D Full-Wave EM Engine, enable current distribution and radiation pattern, then select ok. After simulation all data are save in software directory.

(g) Designing of Microstrip antenna with forth layer

The basic design parameter as design frequency 2.44 GHz, thickness of the patch for first layer 1.6 mm, for second layer 1.6 mm for third layer 4.75 mm and 1.58 mm for forth layer with dielectric coefficient of substrate is 2.55, 4.2, 28.2 and 22 respectively.. Putting these parameters in above equation and calculate length of the patch 26.2 mm and value of width 38.125 mm. The dimension of the feed line calculated directly from the line Gauge of Zeland software for matching 50 Ω , are 21 mm × 4.47 mm and bottom side of patch consider to W_g=W+6h and L_g=L+6h. The design parameters of the patch are indicated in Table 4.

Parameters	Specification	Unit
Patch width	W	38.125 mm
Patch length	L	26.2 mm
Feed line length	F	21 mm
Strip width	Т	4.47 mm
Ground Plane width	\mathbf{W}_{g}	95.305 mm
Ground Plane length	Lg	83.38 mm

Table 4: Design parameters of forth layer antenna at 2.44 GHz.

(h) Simulation of Antenna with Forth Layer by IE3D

Making use of the IE3D software directly and select the Mgrid file, After the selection of Mgrid file then open basic parameter box and select the grid size 0.025 mm, meshing frequency 5 GHz and cell per wavelength = 20, then feed the some parameter before simulation in this dialog box like as top of the surface taking 1.6 mm for first layer, 1.6 mm for second layer, 4.75 for third layer and 1.58 mm for forth layer with dielectric constant 2.55, 4.2, 28.2 and 22 respectively. Now taking loss tangent are 0.025, 0.2, 0.5, and 0.0009 respectively. After the feed above parameters draw the rectangular shape of length 26.2 mm and width 38.125 mm. After draw the patch select the edge of the patch and cut width of cut is 6 mm and depth of cut is 6.5 mm, now draw a straight line with length of 21 mm and width 4.47 mm. After the completion of designing select feed point location and feed at 29.1 mm in \times direction and 0 mm in y direction. On the bottom side of the lower patch design with 83.38 mm \times 95.305 mm metallic ground plane.



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Fig. 6 Proposed antenna with forth layer at 2.44 GHz.

Simulation start with meshing frequency 5 GHz and the range of simulation frequency 0 - 5 GHz with step size 0.01 select the scheme as classical and enable adaptive symmetric matrix solver, simulation engine set as IE3D Full-Wave EM Engine, enable current distribution and radiation pattern, then select ok. After simulation all data are save in software directory.

V. RESULTS AND DISCUSSIONS

(a) Result Analysis of Proposed Antenna with Single Layer

Open the data of reflection coefficient with variation of frequency and add to plot, result of this plot indicates in Figure 7.



Fig. 7 Return loss Vs frequency plot of line feed microstrip antenna at 2.44 GHz.

The applied wave travels into the antenna head and spreads out underneath it. It then reaches the edge of the antenna where some of the energy reflects back and the rest of it radiates out into free-space. The reflected wave then resonates back and forward inside the antenna head until it dies away. Some of this resonant energy returns to the source, some is dissipated in the substrate and the rest of it is radiated out into free-space. If the frequency of the wave is at a resonant point then the electric fields around the edges have maximum amplitude. Thus the radiated electric fields will be at a maximum at resonant frequencies; from Figure 7 the resonance frequency of microstrip antenna is 1.345 GHz. Another calculation the lower frequency and upper frequency corresponding -10 dB reflection coefficient are 1.26 GHz and 1.43 GHz so the bandwidth of 12.639%.



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Table 5: Simulated result of proposed antenna with first layer.

Parameter	Results
Resonance Frequency	1.32 GHz
Return loss	-21.4607 dB
VSWR	1.447237
Bandwidth	12.639 %
Gain	3.34084 dBi
Directivity	4.46192 dBi
Antenna Efficiency	70.2489%
Radiation Efficiency	80.1458%

(b) Result Analysis of Proposed Antenna with Second Layer

Open the data of reflection coefficient with variation of frequency and add to plot, result of this indicates in Figure 8. The applied wave travels into the antenna head and spreads out underneath it. It then reaches the edge of the antenna where some of the energy reflects back and the rest of it radiates out into free-space. The reflected wave then resonates back and forward inside the antenna head until it dies away. Some of this resonant energy returns to the source, some is dissipated in the substrate and the rest of it is radiated out into free-space. If the frequency of the wave is at a resonant point then the electric fields around the edges have maximum amplitude. Thus the radiated electric fields will be at a maximum at resonant frequencies. The resonance frequency of finite ground plane antenna is 1.38 GHz with -23.169 dB reflection coefficient. Another calculation the lower frequency and upper frequency corresponding -10 dB reflection coefficient are 1.27 GHz and 1.48 GHz so the bandwidth of 15.27%



Fig. 8 Return loss Vs frequency plot of proposed microstrip antenna.

Table 6: Simulated result of proposed antenna with second layer.			
Parameter	Antenna with first layer	Antenna with second layer	
Resonance Frequency (GHz)	1.32 GHz	1.38 GHz	
Return loss (dB)	-21.4607 dB	-23.169 dB	
VSWR Bandwidth	1.447237 12.639 %	1.498 15.27%	



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Gain	3.34084 dBi	3.6832 dBi
Directivity	4.46192 dBi	4.41002 dBi
Antenna Efficiency	70.2489%	72.32%
Radiation Efficiency	80.1458%	78.172%

(c) Result Analysis of Proposed Antenna with Third Layer

Open the data of reflection coefficient with variation of frequency and add to plot, result of this indicates in Figure 9.





The applied wave travels into the antenna head and spreads out underneath it. It then reaches the edge of the antenna where some of the energy reflects back and the rest of it radiates out into free-space. The reflected wave then resonates back and forward inside the antenna head until it dies away. Some of this resonant energy returns to the source, some is dissipated in the substrate and the rest of it is radiated out into free-space. If the frequency of the wave is at a resonant point then the electric fields around the edges have maximum amplitude. Thus the radiated electric fields will be at a maximum at resonant frequencies. From Figure 9 the resonance frequency of microstrip antenna is 1.48 GHz. Another calculation the lower frequency and upper frequency corresponding -10 dB reflection coefficient are 1.26 GHz and 1.57 GHz so the bandwidth of 21.9%.

Table 7: Simulated result of proposed antenna with third layer.

Parameter	Antenna with first layer	Antenna with second layer	Antenna with third layer
Resonance Frequency (GHz)	1.32 GHz	1.38 GHz	1.48 GHz
Return loss (dB)	-21.4607 dB	-23.169 dB	-24.778 dB
VSWR	1.45	1.5	1.38
Bandwidth	12.639 %	15.27%	21.9%
Gain	3.34084 dBi	3.6832 dBi	4.1842 dBi
Directivity	4.46192 dBi	4.41002 dBi	3.1102 dBi
Antenna Efficiency	70.2489%	72.32%	75.42%
Radiation Efficiency	80.1458%	78.172%	73.2%

(d) Result Analysis of Proposed Antenna with Forth Layer

Open the data of reflection coefficient with variation of frequency and add to plot, result of this indicates in Figure 10. The applied wave travels into the antenna head and spreads out underneath it. It then reaches the edge of the antenna where some of the energy reflects back and the rest of it radiates out into free-space. The reflected wave then resonates back and forward inside the antenna head until it dies away. Some of this resonant energy returns to the source, some is



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dissipated in the substrate and the rest of it is radiated out into free-space. If the frequency of the wave is at a resonant point then the electric fields around the edges have maximum amplitude. Thus the radiated electric fields will be at a maximum at resonant frequencies. From Figure 10 the resonance frequency of microstrip antenna is 1.46 GHz. Another calculation the lower frequency and upper frequency corresponding -10 dB reflection coefficient are 1.23 GHz and 1.72 GHz so the bandwidth of 33.22%.

VI. CONCLUSION

Based on the computational, analysis of the proposed Microstrip antenna with different layers of dielectric coefficient and calculate their effective dielectric and then design and calculate different parameters but in this paper we focus only on bandwidth calculation. We have enhance bandwidth of increasing layer that is 12.639%, 15.27%, 21.9% and 33.22% respectively up to forth layer.



Fig.10 Return loss Vs frequency plot of proposed microstrip antenna.

Table 8: Simulated result of proposed antenna with forth layer.				
Parameter	Antenna with first layer	Antenna with second layer	Antenna with third layer	Antenna with forth layer
Resonance Frequency (GHz)	1.32 GHz	1.38 GHz	1.48 GHz	1.46 GHz
Return loss (dB)	-21.4607 dB	-23.169 dB	-24.778 dB	-30.65 dB
VSWR	1.45	1.5	1.38	1.56
Bandwidth	12.639 %	15.27%	21.9%	33.22%
Gain	3.34084 dBi	3.6832 dBi	4.1842 dBi	4.88 dBi
Directivity	4.46192 dBi	4.41002 dBi	3.1102 dBi	2.89 dBi
Antenna Efficiency	70.2489%	72.32%	75.42%	80.22%
Radiation Efficiency	80.1458%	78.172%	73.2%	64.13%

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